

電気化学会関西支部 第 51 回電気化学講習会 電気化学の基礎と新しいアプローチ

2. 分極曲線の考え方~腐食、ナトリウムイオン電池、電気二重層キャパシタ、燃料電池~ (その1)

(産業技術総合研究所) 倉谷健太郎

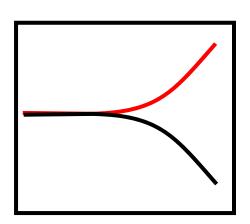
(京都大学) 深見一弘

(大阪大学) 土谷博昭

(鳥取大学) 薄井洋行

(大阪公立大学) 知久昌信

(産業技術総合研究所) 山崎眞一



This supplementary material is the presentation file provided at the 51st Electrochemistry Workshop held by Kansai in response to the comprehensive paper in *Electrochemistry*, **90(10)**, 102003 (2022) https://doi.org/10.5796/electrochemistry.22-66085 entitled,

Electrochemical Polarization Part 1: Fundamentals and Corrosion

Kentaro KURATANI,^{a,*} Kazuhiro FUKAMI,^b Hiroaki TSUCHIYA,^c Hiroyuki USUI,^d Masanobu CHIKU,^e and Shin-ichi YAMAZAKI^a

- ^a Research Institute of Electrochemical Energy, National Institute of Advanced Industrial Science and Technology (AIST), 1-8-31 Midorigaoka, Ikeda, Osaka 563-8577, Japan
- ^b Department of Materials Science and Engineering, Kyoto University, 36-1 Yoshida-Hommachi, Sakyo-ku, Kyoto 606-8501, Japan
- ^c Graduate School of Engineering, Osaka University, 2-1 Yamadaoka, Suita, Osaka 565-0871, Japan
- ^d Graduate School of Engineering, Tottori University, 4-101 Koyama-cho minami, Tottori 680-8552, Japan
- e Graduate School of Engineering, Osaka Metropolitan University, 1-1 Gakuen-cho, Naka-ku, Sakai, Osaka 599-8531, Japan
- * Corresponding author: k-kuratani@aist.go.jp

© The Author(s) 2022. Published by ECSJ. This is an open access material distributed under the terms of the Creative Commons Attribution 4.0 License (CC BY, http://creativecommons.org/licenses/by/4.0/), which permits unrestricted reuse of the work in any medium provided the original work is properly cited. [DOI: 10.50892/data.electrochemistry.20616198].

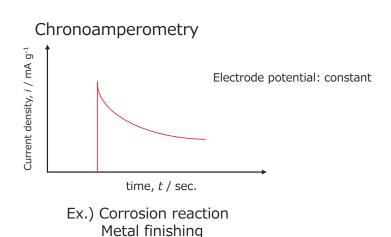


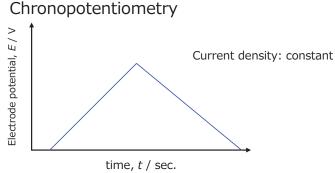
Electrochemical Polarization Part 1: Fundamentals and Corrosion

Kentaro KURATANI,^a Kazuhiro FUKAMI,^b Hiroaki TSUCHIYA,^c Hiroyuki USUI,^d
Masanobu CHIKU,^e Shin-ichi YAMAZAKI^a

Polarization measurements

The term of "chrono" is descended from "chronos", which means "time" in Greek.





Ex.) Charge/discharge reaction

Understanding the correlation between electrode potential and current density is significant to analyze the results obtained from polarization measurement.

^a Research Institute of Electrochemical Energy, National Institute of Advanced Industrial Science and Technology (AIST), 1-8-31, Midorigaoka, Ikeda, Osaka, 563-8577, Japan

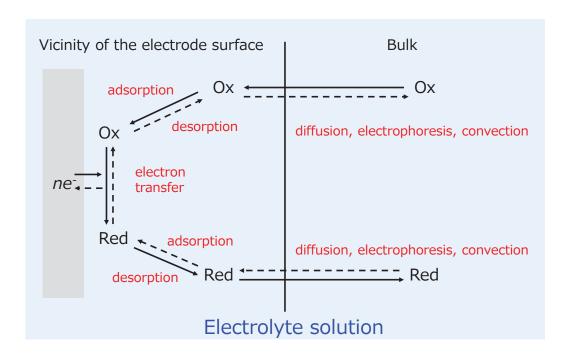
^b Department of Materials Science and Engineering, Kyoto University, 36-1, Yoshida-Hommachi, Sakyo-ku, Kyoto, 606-8501, Japan

^c Graduate School of Engineering, Osaka University, 2-1, Yamadaoka, Suita, Osaka, 565-0871, Japan

^d Graduate School of Engineering, Tottori University, 4-101, Koyama-cho minami, Tottori, 680-8552, Japan

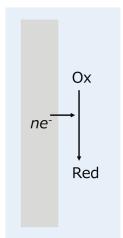
^e Graduate School of Engineering, Osaka Metropolitan University, 1-1, Gakuen-cho, Naka-ku, Sakai, Osaka, 599-8531, Japan

Model of electrode reaction process



Current

Ox + $ne^- \rightarrow \text{Red}$ (Electrochemical reaction under a constant current, I (A), for t (s))



Product mass of Red (mol):
$$N_{\text{Red}}$$
 (mol) = $It/nF = Q/nF$

n: stoichiometric coefficient of electrons in electrochemical reaction

F: Faraday constant (96500 C mol⁻¹)

Q: electric charge generated by the reaction

Reaction rate of Red (mol s⁻¹): $v_t = dN/dt = I/nF$

Reaction rate of Red (mol s⁻¹): $v_t = iS/nF$

I = iS, i: current density, S: electrode square

Reaction rate can be controlled by changing the current density.

Current-potential curve

$$Ox + ne^{-} \stackrel{k_{red}}{\rightleftharpoons} Red \\ k_{ox}$$

$$Ox \\ k_{Red} \stackrel{\uparrow}{\bowtie} k_{Ox} \\ ne^{-} \stackrel{\downarrow}{\longleftarrow} Red$$

$$Red$$

$$AG_{ox}$$

$$AG_{ox}$$

$$v_{\text{red}} = Ac_{\text{ox}} \exp(-\Delta G_{\text{red}}/RT) = k_{\text{red}}c_{\text{ox}}$$

 $v_{\text{ox}} = Ac_{\text{red}} \exp(-\Delta G_{\text{ox}}/RT) = k_{\text{ox}}c_{\text{red}}$

A: frequency factor

 $c_{\rm ox}$: concentration of the reactant near the electrode $c_{\rm red}$: concentration of the product near the electrode $\Delta G_{\rm red}$: activation energy of the reduction reaction $\Delta G_{\rm ox}$: activation energy of the oxidation reaction R: molar gas constant

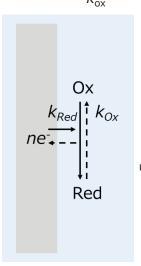
T: absolute temperature

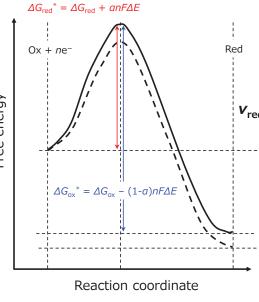
 $k_{\rm red}$: reaction rate constant of the reduction reaction $k_{\rm ox}$: reaction rate constant of the oxidation reaction

Current-potential curve

 $Ox + ne^{-} \overset{k_{\text{red}}}{\rightleftharpoons} Red \\ k_{ox}$

When the potential difference (ΔE) exists at the electrode/electrolyte interface,



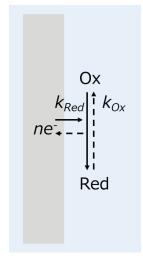


Reaction coordinate

$$\Delta G_{\mathrm{red}}^* = \Delta G_{\mathrm{red}} + anF\Delta E$$
 $a: \text{ transfer coefficient } (0 < a < 1)$
 $v_{\mathrm{red}} = Ac_{\mathrm{ox}} \exp(-\Delta G_{\mathrm{red}}/RT) = k_{\mathrm{red}}c_{\mathrm{ox}}$
 $v_{\mathrm{red}} = Ac_{\mathrm{ox}} \exp(-\Delta G_{\mathrm{red}}^*/RT)$
 $= Ac_{\mathrm{ox}} \exp(-(\Delta G_{\mathrm{red}} + anF\Delta E)/RT)$
 $= Ac_{\mathrm{ox}} (\exp(-\Delta G_{\mathrm{red}}/RT) \times \exp(-anF\Delta E)/RT))$
 $= k_{\mathrm{red}}c_{\mathrm{ox}} \exp(-anF\Delta E)/RT)$

Current-potential curve

$$Ox + ne^{-} \stackrel{k_{red}}{\rightleftharpoons} Red \\ k_{ox}$$



$$v_{\text{red}} = k_{\text{red}} c_{\text{ox}} \exp(-anF\Delta E)/RT$$

This equation can also be edited to current density by multiplying Faraday constant.

$$i_{\text{red}} = Fv_{\text{red}}$$
 $i_{\text{ox}} = Fv_{\text{ox}}$
= $Fk_{\text{red}}c_{\text{ox}}\exp(-anF\Delta E)/RT)$ = $Fk_{\text{ox}}c_{\text{red}}\exp((1-a)nF\Delta E)/RT)$

Under the equilibrium state,
$$i_{red} = i_{ox}$$

$$i_0 = i_{red} = i_{ox}$$
 (exchange current density)

$$= Fk_{\rm red}c_{\rm ox}\exp(-anF\Delta E_{\rm eq})/RT)$$

$$= Fk_{\rm ox}c_{\rm red} \exp((1-a)nF\Delta E_{\rm eq})/RT)$$

Current-potential curve

$$0x + ne^{-} \underset{k_{ox}}{\overset{k_{red}}{\rightleftharpoons}} Red$$

In case the equilibrium state gets out of balance, current flows to the external circuit $(i_{red} \neq i_{ox})$.

Also, we call the potential difference under this situation as overpotential (η) which means the difference of the electrode potential from the equilibrium potential.

$$\begin{array}{c}
Ox \\
k_{Red} \downarrow k_{Ox} \\
ne \downarrow \downarrow \downarrow \\
Red
\end{array}$$

$$i = i_{red} - i_{ox}$$

$$= Fk_{red}c_{ox}exp(-anF(\Delta E_{eq} + \eta)/RT)$$

$$- Fk_{ox}c_{red}exp((1-a)nF(\Delta E_{eq} + \eta)/RT)$$

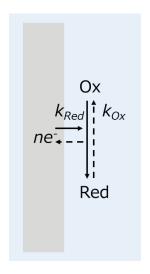
$$= i_0[exp(-anF\eta/RT) - exp((1-a)nF\eta/RT)]$$

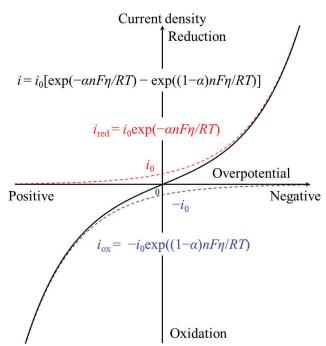
Butler-Volmer equation

Current-potential curve based on Butler-Volmer equation

$$0x + ne^{-} \stackrel{k_{\text{red}}}{\rightleftharpoons} \text{Red}$$

$$k_{\text{ox}}$$

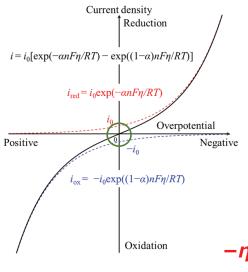




Current-potential curve

In case of $|\eta|$ <5 mV

$$i = i_0[\exp(-anF\eta/RT) - \exp((1-a)nF\eta/RT)]$$



Taylor expansion
$$e^{x} = 1 + \frac{x}{1!} + \frac{x^{2}}{2!} + \frac{x^{3}}{3!} + \cdots, \quad -\infty < x < \infty$$

$$e^{x} = 1 + x$$

$$i = i_0[1 + (-anF\eta/RT) - (1 + (1-a)nF\eta/RT)]$$

$$= i_0(nF\eta/RT)$$

$$\eta = -(RT/i_0 nF)i$$

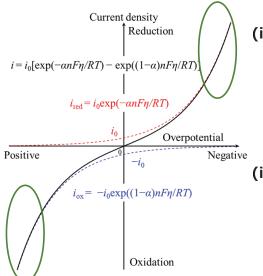
$$-\eta/i = RT/i_0 nF$$

= R_{ct} (R_{ct} : charge transfer resistance)

Current-potential curve

In case of $|\eta|$ > 70 mV

$$i = i_0[\exp(-anF\eta/RT) - \exp((1-a)nF\eta/RT)]$$



(i)
$$\eta$$
 < -70 mV (the term i_{ox} is negligible.)

$$i = i_0 \exp(-anF\eta/RT)$$

$$\eta = (RT \ln i_0)/anF - (RT \ln i)/anF$$

$$= 2.303RT\log i_0/anF - 2.303RT\log i/anF$$

(ii)
$$\eta > +70$$
 mV (the term i_{red} is negligible.)

$$i = -i_0 \exp((1-a)nF\eta/RT) = |i_0| \exp((1-a)nF\eta/RT)$$

$$\eta = -(RT | \text{ln} i_0)/(1-a)nF + (RT | \text{ln} i)/(1-a)nF$$

$$= -2.303RT\log i_0/(1-a)nF - 2.303RT\log i/(1-a)nF$$

Tafel plot

Ox + $ne^{-\frac{k_{red}}{\rightleftharpoons}}$ Red k_{ox} Slope: $-\alpha nF/2.303RT$ Slope: $(1-\alpha nF/2.303RT)$ Slope:

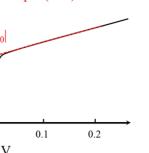
(i)
$$\eta < -70$$
 mV (the term i_{ox} is negligible.)

$$\eta = 2.303RT\log i_0/anF - 2.303RT\log i/anF$$

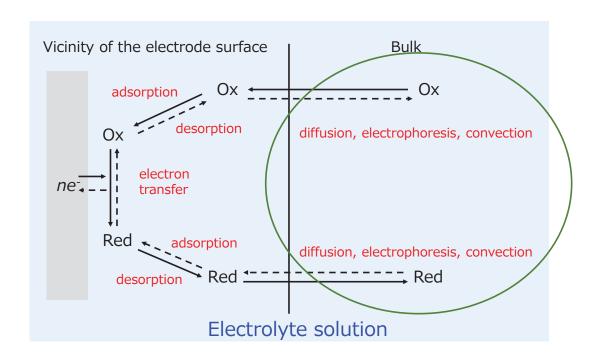
(ii)
$$\eta > -70$$
 mV (the term i_{ox} is negligible.)

$$\eta = -2.303RT\log i_0/(1-a)nF - 2.303RT\log i/(1-a)nF$$

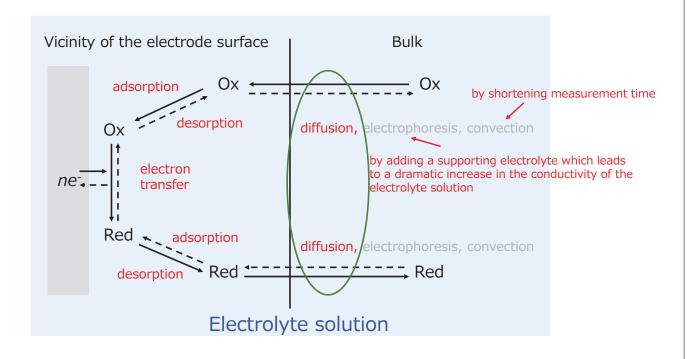
Slope: $(1-\alpha)nF/2.303RT$ Tafel equation $(\eta=a\pm b\log i)$



Model of electrode reaction process



Model of electrode reaction process



Mass transfer

 $Ox + ne^- \rightarrow Red$

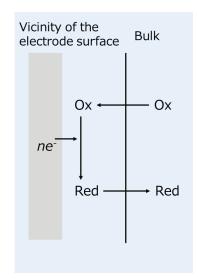
Concentration, c

Slope: $(c_{\text{bulk}}-c_0)/\delta$

 c_0

 δ

Nernst diffusion layer



Fick's first law

$$J = -D(dc_{\text{bulk}}/dx)$$

 C_0 : concentration of the reactant at x = 0

D: diffusion constant
J: diffusion flux

$$J = -D(c_{\text{bulk}} - c_0)/\delta$$

Diffusion flux is mole number that passes through a unit area of cross-section in a unit time

$$i = -nFD(c_{\text{bulk}} - c_0)/\delta$$

When the concentration of the reactant near the electrode becomes 0 ($C_0 = 0$)

Distance, x $i = -nFD(c_{\text{bulk}})/\delta$

Diffusion-limiting current density

Electrochemical Polarization Part 1: Fundamentals and Corrosion

Electrochemical Polarization in Fundamental Corrosion Research

Kentaro Kuratani,^a Kazuhiro Fukami,^b Hiroaki Tsuchiya,^c Hiroyuki Usui,^d Masanobu Chiku,^e Shin-ichi Yamazaki^a

Equilibrium and Steady State

Equilibrium

Consider a half-cell reaction

ex.)
$$M^{2+} + 2e^{-} = M$$

The equilibrium potential is expressed by the Nernst equation.

$$E_{\rm M^{2+}/M} = E_{\rm M^{2+}/M}^{\circ} - \frac{RT}{2F} \ln \frac{1}{a_{\rm M^{2+}}}$$

Steady state

Two half-cell reactions are coupled.

ex.)
$$M^{2+} + 2e^{-} \leftarrow M$$

2 $H^{+} + 2e^{-} \rightarrow H_{2}$

^a Research Institute of Electrochemical Energy, National Institute of Advanced Industrial Science and Technology (AIST), 1-8-31, Midorigaoka, Ikeda, Osaka, 563-8577, Japan

^b Department of Materials Science and Engineering, Kyoto University, 36-1, Yoshida-Hommachi, Sakyo-ku, Kyoto, 606-8501, Japan

c Graduate School of Engineering, Osaka University, 2-1, Yamadaoka, Suita, Osaka, 565-0871, Japan

d Graduate School of Engineering, Tottori University, 4-101, Koyama-cho minami, Tottori, 680-8552, Japan

^e Graduate School of Engineering, Osaka Metropolitan University, 1-1, Gakuen-cho, Naka-ku, Sakai, Osaka, 599-8531, Japan

Equilibrium and Steady State

Steady state

Equilibrium potentials of the two reactions

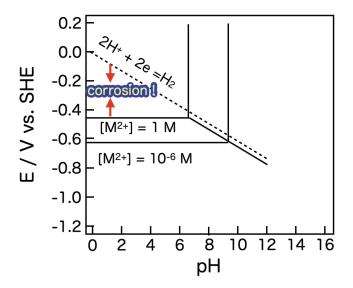
$$E_{\rm M^{2+}/M} = E_{\rm M^{2+}/M}^{\circ} - \frac{RT}{2F} \ln \frac{1}{a_{\rm M^{2+}}}$$

$$E_{\text{H}^+/\text{H}_2} = E_{\text{H}^+/\text{H}_2}^{\circ} - \frac{RT}{2F} \ln \frac{1}{a_{\text{H}^+}^2}$$

The corrosion of M occurs when the *emf* of the coupled reaction is positive ($\triangle G$ is negative).

Potential-pH diagrams are helpful to judge thermodynamically whether a corrosion reaction of interest occurs or not.

Potential-pH diagram (Pourbaix diagram)

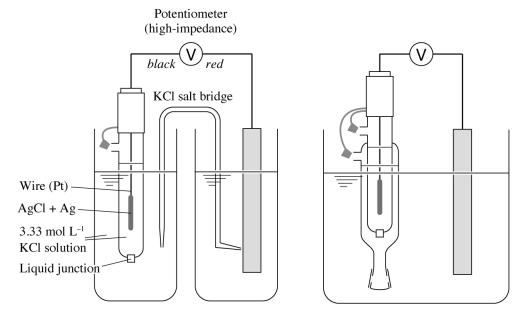


Potential-pH diagram gives information whether the corrosion thermodynamically occurs or not.

To understand the corrosion quantitatively, evaluation by stationary polarization is necessary.

Electrochemical measurements

Measurement for corrosion potential

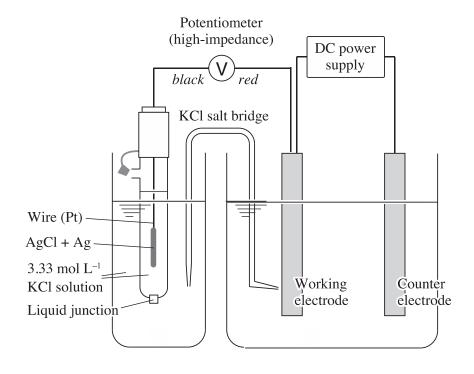


When the contamination of Cl⁻ is not allowed, a double-junction type reference electrode or a reference electrode without Cl⁻ should be used.

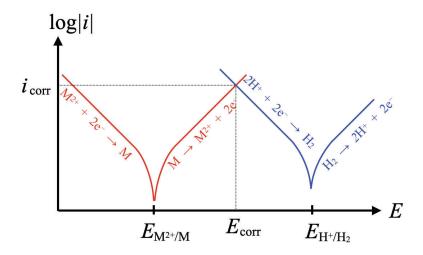
(ex. Hg|Hg₂SO₄ in an acidic solution and Hg|HgO in an alkaline solution)

Electrochemical measurements

Measurement for stationary polarization



Stationary polarization curves

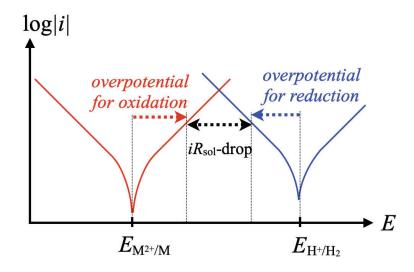


The current density for the oxidation of M is equal to that for the reduction of H^+ to H_2 at the potential denoted as $E_{\rm corr}$.

 $E_{\rm corr}$ is the corrosion potential, while $i_{\rm corr}$ is the corrosion current density.

Effect of iR_{sol} -drop in solution on corrosion rate

The iR_{sol} -drop in the test solution must be considered to discuss corrosion behavior quantitatively.



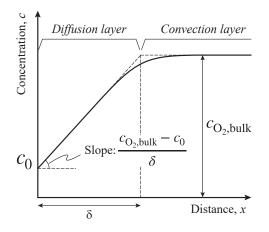
The overpotential for the oxidation of M decreases when the conductivity of the test solution is not high.

Effect of mass-transfer on corrosion rate

In corrosion reactions, the reduction reaction can be the oxygen reduction to water.

$$M^{2+} + 2e^{-} = M$$

 $O_{2} + 2H_{2}O + 4e^{-} = 4OH^{-}$

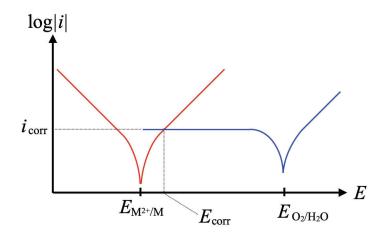


The concentration of dissolved oxygen is low.

The oxygen reduction takes place under diffusion-limited condition. (expressed by the Cottrel equation)

$$\left|i_{\mathrm{O}_{2},\mathrm{diff}}\right| = \frac{4FD_{\mathrm{O}_{2}}c_{\mathrm{O}_{2},\mathrm{bulk}}}{\delta}$$

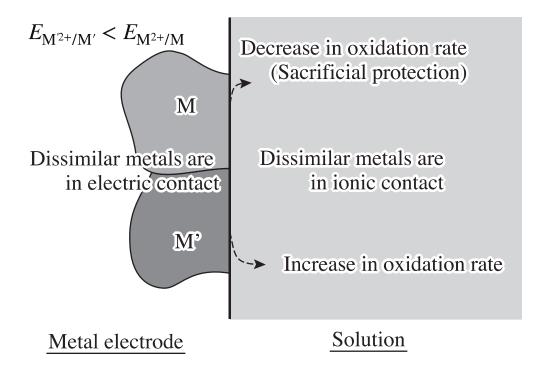
Effect of mass-transfer on corrosion rate



 $E_{
m corr}$ is determined as the potential where the oxidation of M and the reduction of oxygen is balanced each other.

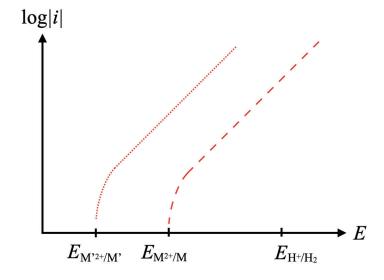
Since the current density of oxygen reduction reaches its maximum, i_{corr} is equal to that of oxygen reduction.

What is galvanic corrosion?



Galvanic corrosion

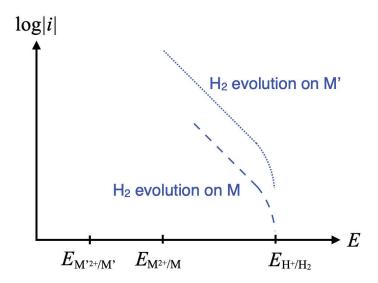
The oxidation reactions (dissolution) of M and M'



The oxidation of the metals occurs when the applied potential is more positive than the equilibrium potentials (Butler-Volmer equation).

Galvanic corrosion

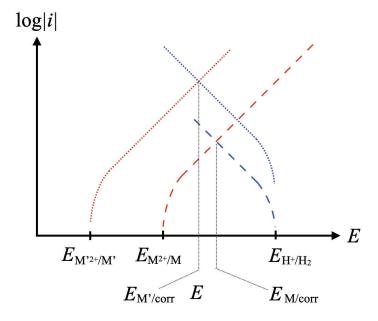
The reduction reactions (H₂ evolution) on M and M'



Since the exchange current density for the H_2 evolution depends on metal used as an electrode, two different curves are plotted from $E_{\mathrm{H^+\!/H_2}}$.

Galvanic corrosion

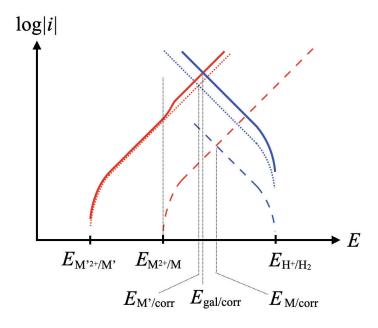
Corrosion potentials without electric contact



Without electric contact, the corrosion occurs on each metal even when M and M' are immersed in a common solution.

Galvanic corrosion

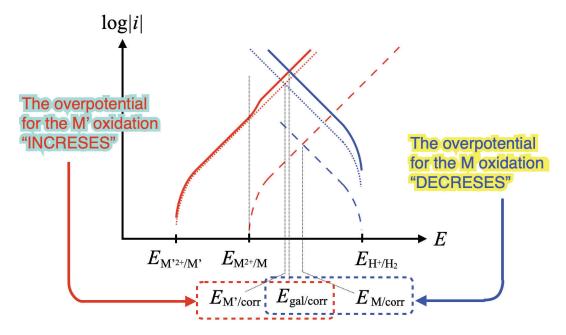
Corrosion potentials with both electric and ionic contact



The corrosion potential $E_{\rm gal/corr}$ is determined by both the total current density of oxidation and that of reduction.

Galvanic corrosion

Sacrificial protection



The sacrificial protection of M is expected since the overpotential for the M oxidation decreases when M and M' in both electric and ionic contacts.